

## A Time Resolved Powder Neutron Diffraction Investigation of Reactions of Portland Cement Components with Water

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The reactions between D<sub>2</sub>O and the Portland cement clinker components Ca<sub>3</sub>SiO<sub>5</sub>, β-Ca<sub>2</sub>SiO<sub>4</sub>, and Ca<sub>2</sub>AlFeO<sub>5</sub> were investigated by on-line powder neutron diffraction methods at temperatures up to 120 °C. The only crystalline reaction product found in the reaction of Ca<sub>3</sub>SiO<sub>5</sub> with water is Ca(OD)<sub>2</sub>. The reaction of β-Ca<sub>2</sub>SiO<sub>4</sub> is much slower than that of Ca<sub>3</sub>SiO<sub>5</sub>. The crystalline reaction products of the reaction of Ca<sub>2</sub>AlFeO<sub>5</sub> with water are Ca(OD)<sub>2</sub> and Ca<sub>3</sub>Al<sub>2</sub>(OD)<sub>12</sub>. The activation energy for the formation of Ca<sub>3</sub>Al<sub>2</sub>(OD)<sub>12</sub> in the Ca<sub>2</sub>AlFeO<sub>5</sub>-D<sub>2</sub>O reaction is 58.2 kJ/mol.

The reaction rates of hydration for compounds of the type Ca<sub>x</sub>Al<sub>y</sub>O<sub>z</sub> are related to the relative content of calcium ions. Compounds with high calcium content react faster with water than compounds with low calcium content. Some correlations between reactivity and crystal structures are discussed.

Heterogeneous mixtures of solids and water described as cement pastes or cement mortars comprise a wide range of chemical systems, each with typical ways of reaction. This work is restricted to hydration reactions of solid compounds relevant to Portland cement clinker. This material, however, shows wide variations with respect to composition due to differences between available raw materials. The main components (oxides) of two representative types of cement clinker are given in Table 1. Tricalcium silicate Ca<sub>3</sub>SiO<sub>5</sub>, dicalcium silicate β-Ca<sub>2</sub>SiO<sub>4</sub>, tricalcium aluminate Ca<sub>3</sub>Al<sub>2</sub>O<sub>6</sub>, and Brownmillerite Ca<sub>2</sub>AlFeO<sub>5</sub>, are the main components. In contact with water these crystalline phases generally undergo hydration reactions yielding new crystalline hydrated phases and amorphous gels.<sup>2,3</sup> These processes in the cement mortars provoke solidification during a few hours, whereas the final strength properties are only attained after a number of weeks.

Table 1. Representative compositions (%) of Portland cement clinker (Aalborg Portland).<sup>1</sup>

Oxides	Low-alkali cement	Rapid cement
Ca <sub>3</sub> SiO <sub>5</sub>	60	58
Ca <sub>2</sub> SiO <sub>4</sub>	26	20
Ca <sub>3</sub> Al <sub>2</sub> O <sub>6</sub>	1.5	8.6
Ca <sub>2</sub> AlFeO <sub>5</sub>	9.2	9.0
CaO (free)	0.6	1.1

Table 2. Short-hand notations for mixed oxides and hydroxides discussed in the text.

$C_3S \equiv Ca_3SiO_5$	$C_3A \equiv Ca_3Al_2O_6$	$CA \equiv CaAl_2O_4$
$\beta-C_2S \equiv \beta-Ca_2SiO_4$	$C_{12}A_7 \equiv Ca_{12}Al_{14}O_{33}$	$CA_2 \equiv CaAl_4O_7$
$C_4AF \equiv Ca_2AlFeO_5$	$C_5A_3 \equiv Ca_5Al_6O_{14}$	$C_3AD_6 \equiv Ca_3Al_2(OD)_{12}$

The results of a study of reactions between water and the pure calcium oxides  $Ca_3Al_2O_6$ ,  $Ca_{12}Al_{14}O_{33}$ ,  $CaAl_2O_4$ , and  $CaAl_4O_7$  were published in Ref. 4. Due to the large number of simultaneous reactions it is difficult to ascribe measured quantities to a particular chemical reaction for Portland cement. Hence, in this investigation the more convenient approach of studying reactions between water and some pure oxides was first adopted. As a second step, different additives were included into these reactions. The outcome of the latter studies will be published separately. A large number of investigations on hydration of Portland cement mortars and on selected cement clinker compounds have been reported using a variety of methods (e.g. measurements of heat evolution,<sup>5</sup> X-ray diffraction,<sup>6</sup> small-angle scattering,<sup>7</sup> SEM,<sup>8,9</sup> TEM<sup>8,9,10</sup> and registration of mechanical properties<sup>11</sup>). In many cases the reaction products have only been studied at certain time intervals after having been brought to ambient conditions.

This work deals with the hydration properties of  $Ca_3SiO_5$ ,  $\beta-Ca_2SiO_4$ , and  $Ca_2AlFeO_5$ . In the present investigation, using on-line powder neutron diffraction measurements of characteristic scattered intensities from reactants and products, the chemical changes are recorded in real time and the chemical reactions proceed in the sample holder simultaneously with the diffraction measurements.

The abbreviations commonly used in cement chemistry literature by referring to the compositions in terms of double oxides, are adopted. Setting *C* for CaO, *A* for  $Al_2O_3$ , *F* for  $Fe_2O_3$ , *S* for  $SiO_2$ , and *D* for  $D_2O$  (*H* for  $H_2O$ ) the short hand notation for the relevant phases are as listed in Table 2.

## EXPERIMENTAL

(i) *Sample preparation and characterization.*  $C_4AF$  was made by zone melting of stoichiometric mixtures of the oxides in a crystal growth furnace. Chemicals used were  $Al_2O_3$ ,  $Fe_2O_3$  (Merck, analytical grade) and CaO made from  $CaCO_3$  (Merck, analytical grade). The calcium carbonate was kept for 8 h at 1000 °C in a crucible furnace to produce CaO.

It turned out to be impossible to synthesize  $C_3S$  and  $\beta-C_2S$  from stoichiometric amounts of the pure oxides CaO and  $SiO_2$  (amorphous, Elkem). This is in accordance with the fact that  $C_3S$  is metastable below 1250 °C, while pure  $\beta-C_2S$  is metastable relative to  $\gamma-C_2S$  below 675 °C but can be stabilized by minor quantities of oxide additives. The calcium silicates in cement clinker contain minor amounts of other oxides that act as stabilizers for  $C_3S$  and  $\beta-C_2S$ . The present  $C_3S$  sample was made from a mixture of 0.71 mol CaO, 0.23 mol amorphous  $SiO_2$ , 0.006 mol  $\gamma-FeOOH$  (Minnesota Mining and Manufacturing Company), 0.005 mol  $Al_2O_3$ , 0.025 mol MgO (Lycal, technical grade), and 0.011 mol  $MnF_2$  (Riedel, technical grade), corresponding to a product which is quoted as "Alite"; it will, however, be denoted as  $C_3S$  here. The finely ground mixtures of these compounds were heated in a MgO crucible at 1440 °C for 20 h. The advantage of using amorphous  $SiO_2$  is increased reactivity, the additions of MgO,  $Fe_2O_3$ , and  $Al_2O_3$  stabilize the  $C_3S$  phase while the presence of manganese fluoride reduces the formation temperature to approximately 1100 °C.<sup>13</sup>

$\beta-C_2S$  was made similarly from a mixture of 0.40 mol CaO, 0.17 mol crystalline  $SiO_2$  (Merck, analytical grade), 0.7 mmol  $Al_2O_3$ , and 0.4 mmol  $Fe_2O_3$ . After crushing and

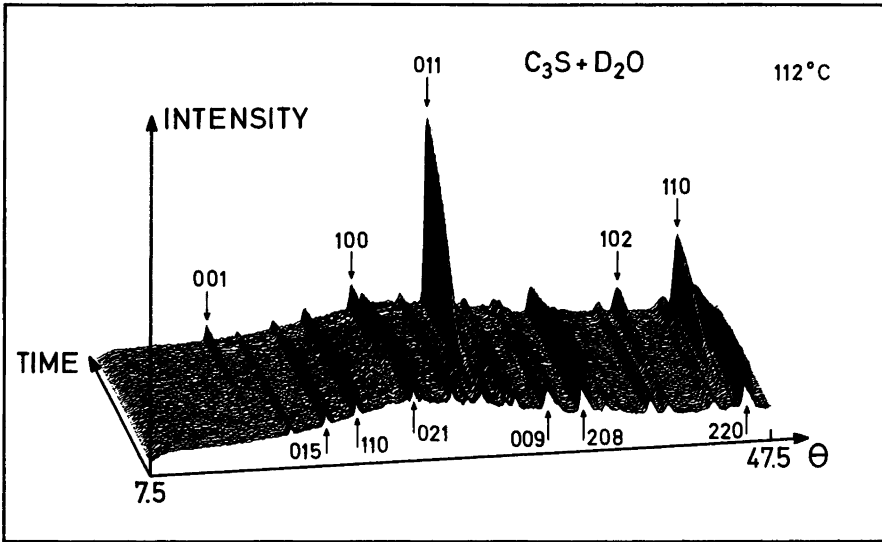


Fig. 1. Powder neutron diffraction diagrams of  $C_3S$ - $D_2O$  mixture at  $112^\circ C$  recorded with 20 min intervals. Miller indices for selected reflections of  $C_3S$   $\uparrow$  (refer to pseudocell) and  $Ca(OD)_2$   $\downarrow$  are indicated.

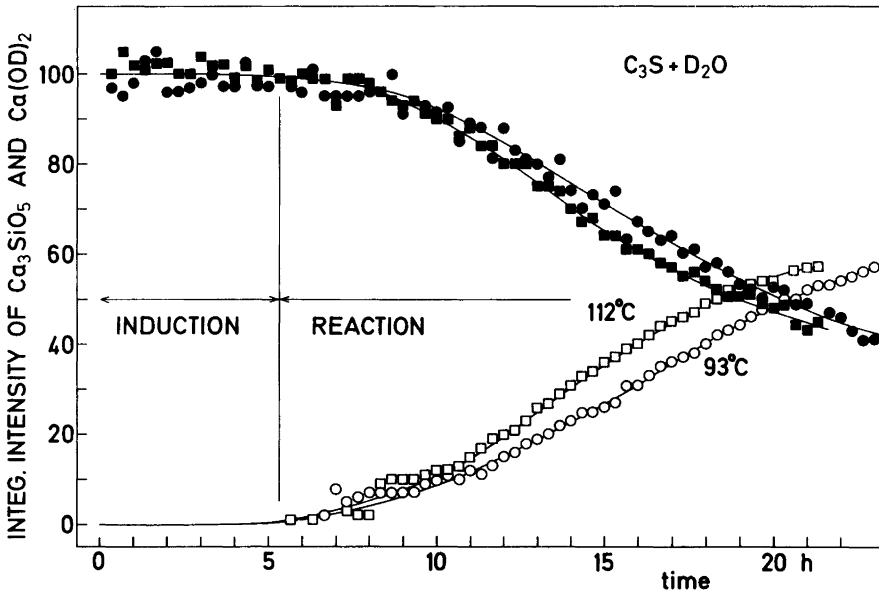


Fig. 2. Integrated intensities of  $C_3S$  ( $\bullet$ ,  $\blacksquare$ ) and  $Ca(OD)_2$  ( $\circ$ ,  $\square$ ) vs. time for the reaction of  $C_3S$  with  $D_2O$  at 93 and  $112^\circ C$ . The intensities of  $C_3S$  and  $Ca(OD)_2$  are on relative scales. Estimated uncertainty 4 %.

mixing, the products were pressed isostatically to 5 cm long rods that were heated in MgO crucibles in a furnace at 1315 °C for 48 h. Upon cooling, the rods broke down as powders due to the conversion of  $\alpha$ - $C_2S$  into  $\gamma$ - $C_2S$ . This powder was reheated in order to increase the  $\beta$ - $C_2S/\gamma$ - $C_2S$  ratio,<sup>14</sup> first at 400 °C for 8 h, next at 1000 °C for 8 h. This heat treatment was repeated once and the sample was finally kept at 400 °C for 8 h before cooling to room temperature over 1 h. At that stage the sample contained only minor impurities of  $\gamma$ - $C_2S$  and CaO.

The fractions of the samples which passed a 150 mesh sieve were used for the hydration experiments studied by on-line neutron diffraction. No further information on the particle size is at hand. The quality of the starting materials was checked by Guinier photographs using  $CuK\alpha_1$  radiation and Si as internal standard. All starting materials gave sharp Guinier photographs. X-Ray powder diffraction data were also recorded for the end products of the hydration experiments.

(ii) *Powder neutron diffraction.* Powder neutron diffraction data were collected on the D1B diffractometer at the Laue-Langevin Institute, using neutrons of wavelength 2.517 Å (evaluated using  $C_{12}A_7$  as standard;  $a=11.989(1)$  Å). The diffractometer has a 400-cell multidetector covering 80° in  $2\theta$ . In a typical experiment, 3.00 g solid was mixed with 3.75 ml  $D_2O$  (99.7%) in an 11 mm-diameter vanadium container. The container, sealed with an indium gasket, was placed in a thermostated vanadium oven with a temperature stability of  $\pm 1$  °C. The large sample and beam size ensure representative measurements of the bulk reactions, which otherwise might be a problem in experiments using X-ray radiation. The recorded intensities were extracted at 5, 10 or 20 min intervals, depending on the actual reaction rate. The evolution in real time of a chemical reaction is visualized<sup>15</sup> in Fig. 1, which shows how the intensities of Bragg reflections from the crystalline starting material  $C_3S$  and the reaction product  $Ca(OD)_2$  change in time. Miller indices are given for selected Bragg peaks. The main features of such reactions can equally well be presented as the time dependence of integrated intensities<sup>16</sup> of selected reflections. This is exemplified in Fig. 2.

## RESULTS

(i) *Hydration of calcium silicates.* The hydration of  $C_3S$  can generally be divided into three steps,<sup>17,18</sup> respectively denoted initialization, induction and reaction ranges, cf. Fig. 2.

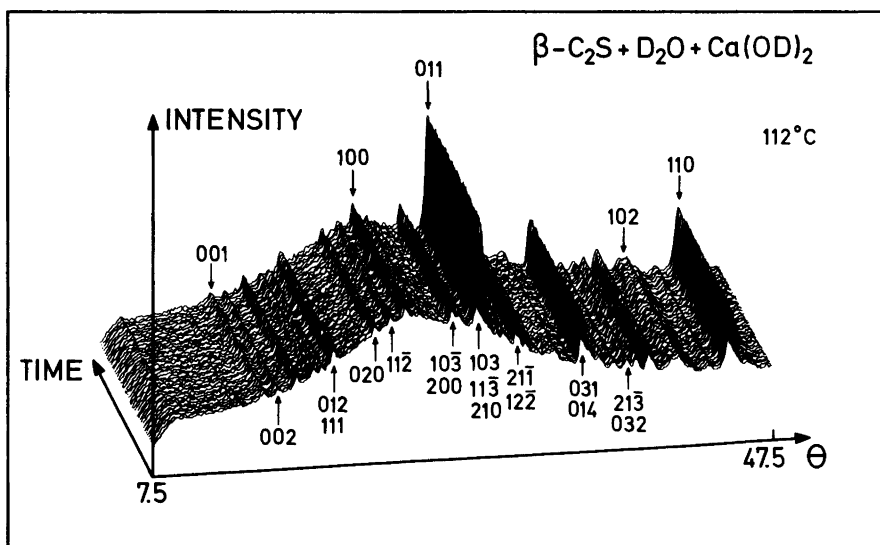
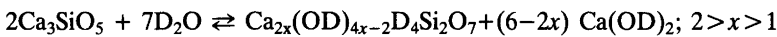


Fig. 3. Powder neutron diffraction diagrams of a  $\beta$ - $C_2S$ - $Ca(OD)_2$ - $D_2O$  mixture at 112 °C recorded with 20 min intervals. Miller indices for  $\beta$ - $C_2S$   $\uparrow$  and  $Ca(OD)_2$   $\downarrow$  are included.

According to Refs. 17, 18 a rapid dissolution of a small amount of  $C_3S$  takes place in the initialization step immediately after the solid is brought in contact with water. However, the  $C_3S$  amount consumed in this step is so small (1–2 %) that it could not be resolved in the present experiment. At least two explanations for the following induction (dormant) period prevail;<sup>19</sup> either a reduced nucleation rate of hydration products [amorphous  $C-S-D$  gel and  $Ca(OD)_2$ ] is the cause, or else the presence of a protective layer surrounding the grains for a certain time explains the facts. The onset of the reaction period, after 5–6 h, is characterized by precipitation of  $Ca(OD)_2$ .

$Ca(OD)_2$  is the only crystalline reaction product, *cf.* Figs. 1 and 2. In Fig. 2 the intensities of  $Ca(OD)_2$  have been normalized to 50 for the measured value 50 of the  $C_3S$  intensity, assuming equal reaction rates for the precipitation of  $Ca(OD)_2$  and the dissolution of  $C_3S$ . The total reaction can be written as<sup>20</sup>



All 'silicon oxide' from the dissolution of  $C_3S$  is found in the amorphous  $C-S-D$  gels. The hydration rate attains its maximum value during the reaction periods investigated. The maximum is shifted towards longer times by reducing the temperature, *viz.* at ~ 12 and ~ 17 h for 112 and 93 °C, respectively. When discussing the hydration properties of  $C_3S$  attention should be paid to the fact that the amount of impurities introduced during the syntheses will affect the reactivity.

For  $\beta-C_2S$  the hydration rate is less than for  $C_3S$  in conformity with earlier findings.<sup>21,22</sup> Fig. 3 shows the real time evolution of the diffraction pattern of a mixture of  $\beta-C_2S/Ca(OD)_2/D_2O$  at 112 °C and only minor changes are observed. Similar data collected at 102 and 120 °C confirm these findings.

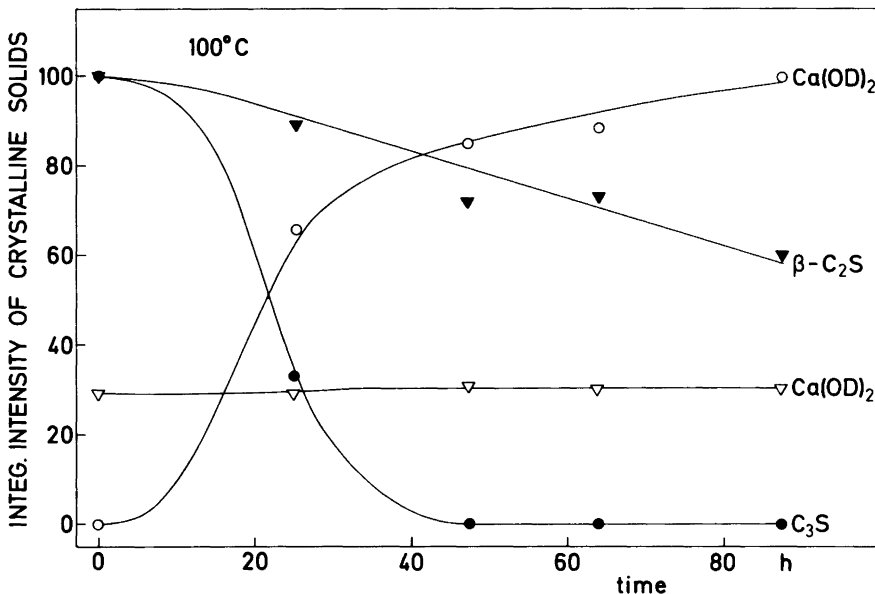


Fig. 4. Integrated intensity of  $C_3S$  (●),  $\beta-C_2S$  (▼) and  $Ca(OD)_2$  (○,▽) vs. time for reactions between  $C_3S$  and  $D_2O$  or  $\beta-C_2S$  and  $D_2O$  at 100 °C.

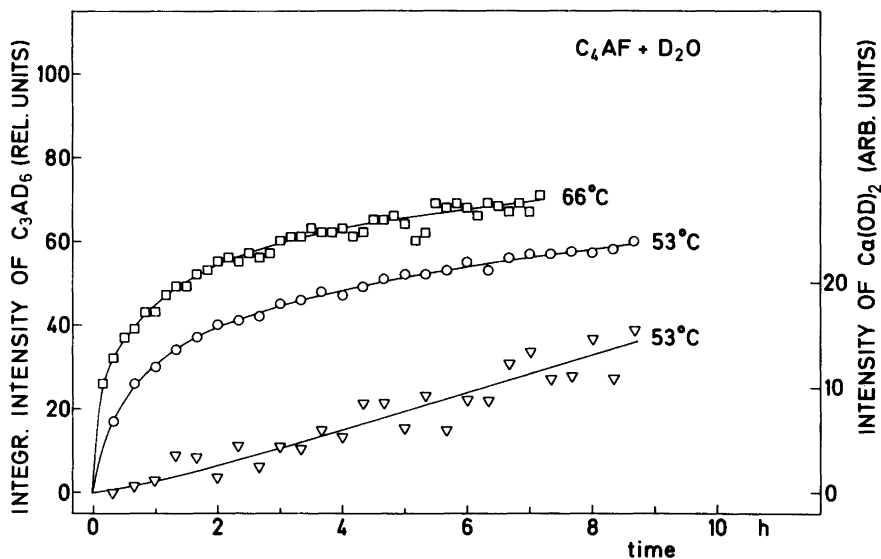


Fig. 5. Integrated intensity of  $C_3AD_6$  (○, □) vs. time for reactions between  $C_4AF$  and  $D_2O$  at 53 and 66 °C. A representative curve for the crystallization of  $Ca(OD)_2$  (at 53 °C) is included (▽).

In order to obtain data for longer hydration times than allowed by an on-line experiment, relevant sample mixtures containing  $C_3S$ ,  $\beta$ - $C_2S$  (with a small  $Ca(OD)_2$  excess) and  $D_2O$  were heated at 100 °C for longer periods of time. The heat treatments were only interrupted for the time necessary to record powder neutron diffraction intensities. The results in Fig. 4 show that  $\beta$ - $C_2S$  reacts more slowly with  $D_2O$  than does  $C_3S$ .

(ii) *Hydration of Brownmillerite.* Brownmillerite,  $C_4AF$  belongs to a solid solution series comprising  $CaO$ ,  $Al_2O_3$ , and  $Fe_2O_3$  [ $Ca_4(Al_xFe_{1-x})_4O_{10} \equiv C_4A_{2x}F_{2-2x}$ ;  $x \leq 0.69$ ]. The hydration properties of the phase are reported to vary slightly with composition ( $x$ ). The reaction rates are higher for  $A$  rich samples. Other  $C$ - $F$  phases like  $CF$ ,  $CF_2$  were not studied since they are not relevant for the properties of Portland cement. The refined unit cell parameters for the  $C_4AF$  sample used is  $a=5.546(1)$ ,  $b=14.460(3)$ ,  $c=5.325(1)$  Å; space group  $Ibm2$ , indexing based on calculated intensities using the program LAZY-PULVERIX.<sup>23</sup> The unit cell dimensions obtained correspond to samples more rich in  $A$  than  $C_4AF$  according to Refs. 24, 25.

Results from the hydration experiments of  $C_4AF$  are displayed in Figs. 5 and 6. At temperatures between 53 and 103 °C, one of the crystalline reaction products is a cubic phase ( $C_3AD_6$ ) of the hydrogarnet type.<sup>26,27</sup> When  $C_4AF$  is brought in contact with water, the integrated intensities of  $C_4AF$  reflections are, during a short time, reduced significantly, and  $C_4AF$  resembles in this manner  $C_3A$ . A small amount of  $C_4AF$  remained unreacted throughout the experiments, probably because large grains become protected by rapid overgrowth of reaction products. The curve in Fig. 6 for  $C_4AF$  at 103 °C is representative for all the  $C_4AF$  experiments.  $C_3AD_6$  (hydrogrossular) is the main reaction product from hydrolysis of calcium aluminates, however it forms easily solid solution series, among these  $Ca_3Al_{2-x}Fe_x(OD)_{12}$ . Least-squares refinements based on Guinier photographs of a  $C_4AF$  sample completely hydrolysed at 80 °C for 48 h give a cell constant  $a=12.592(1)$  compared to

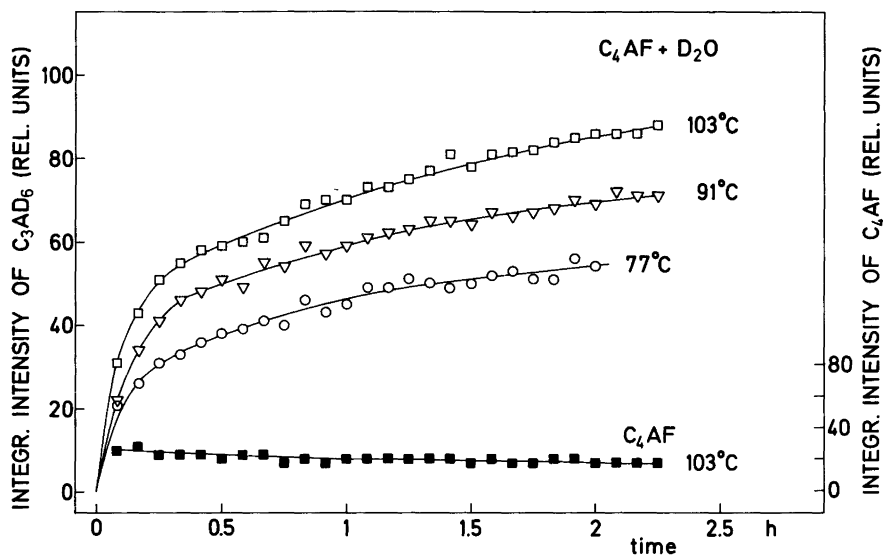


Fig. 6. Integrated intensity of  $C_4AF$  (■) and  $C_3AD_6$  (○, ▽, □) vs. time for reactions between  $C_4AF$  and  $D_2O$  at 77, 91, and 103 °C.

12.571(2) Å for pure  $C_3AD_6$ . This is in agreement with corresponding values derived from the neutron diffraction data ( $a=12.635(3)$  and 12.574(2) Å) and indicates that the obtained reaction product contains only slight amounts of iron. The unit cell parameter for  $Ca_3Al_{2-x}Fe_x(OD)_{12}$  is reported to vary approximately linearly with  $x$ , being 12.76 Å for  $C_3FD_6$ .<sup>28</sup> A comparison of observed and calculated Bragg intensities of the solid solution phase further confirmed the reaction products to be  $C_3AD_6$  and  $Ca(OD)_2$ . The precipitation of  $Ca(OD)_2$  also suggests that nearly all Fe will be in the amorphous part of the sample, as calcium would otherwise be used in the formation of  $C_3FD_6$  or of  $Ca_3Al_{2-x}Fe_x(OD)_{12}$  with a high content of Fe:  $C_4AF+7D_2O \rightarrow C_3AD_6 + Ca(OD)_2 + "Fe_2O_3"$  (amorphous). In this respect, Brownmillerite differs from  $C_3A$  since the latter does not precipitate  $Ca(OD)_2$  upon hydrolysis.<sup>4</sup>

## DISCUSSION

The powder neutron diffraction studies show that the hydration properties of  $C-A^*$ ,  $C-S$ , and  $C-A-F$  phases differ considerably. A measure of the reactivity in the hydration of a compound is the time ( $t_{0.5}$ ) required for consumption (production) of half of the amount of reactants (products). Table 3 presents the results of  $t_{0.5}$  deduced from the neutron diffraction studies. In a number of cases are  $t_{0.5}$  (product) >  $t_{0.5}$  (reactant), that is the reactants are nearly completely consumed before any crystalline products are observed. This is the case for  $C_3A$ ,  $C_4AF$ , and to a less pronounced extend for  $CA$ . It is observed that the values of  $t_{0.5}$  (reactant) decreases with increasing  $C/A$  ratio in the  $C-A$  series of compounds. The reduced reactivity of  $C-S$  phases relative to  $C-A$  phases are evident from the corresponding  $t_{0.5}$  values. The hydration reactions of  $C_3S$ ,  $CA_2$ , and possibly as well of  $CA$  are characterized by

\* The compound  $C_{12}A_7$  was erroneously quoted as  $C_5A_3$  in Ref. 4.

Table 3. Time ( $h$ ) necessary for reducing (increasing) the quantity of reactants (products) to half their maximum value.

Starting material	$T(^{\circ}\text{C})$	$t_{0.5}(\text{reactant})$	$t_{0.5}(\text{product})$
$\text{C}_3\text{S}$	93	20.3	$\sim 20$
$\beta\text{-C}_2\text{S}$	100	$\sim 100$	$\gg 100$
$\text{C}_4\text{AF}$	53	0.5	4.6
	66	0.4	1.5
$\text{C}_3\text{A}$	49	$< 0.1$	0.3
	63	$< 0.1$	0.12
$\text{C}_{12}\text{A}_7$	49	1.9	2.0
	63	0.3	0.3
$\text{CA}$	49	3.5	$> 7.0$
	63	1.3	3.5
$\text{CA}_2$	49	$50.0^a$	$> 50.0^a$
	93	3.5	3.5

<sup>a</sup> Extrapolated.

an induction period. The reason for this has been discussed above. The large span in  $t_{0.5}$  values for the various main constituents of Portland cement clinker (*cf.* Tables 1 and 3) are reflected in time dependent mechanical properties of the end products.

A more detailed understanding of the nature of the reactions is gained from a study of the time dependence of  $\alpha(t)$ , where  $\alpha(t)$  is the degree of hydration at time  $t$ . The reactions are heterogeneous between water and powdered materials. In this case, the changing geometry of the reaction interfaces and diffusion paths will dominate the reaction rate expressions. When the reaction interface moves at a constant rate, the kinetics are said to be linear and the rate varies as the area of the reaction interface. Parabolic kinetics involve a rate control by mass transport through a layer on the particle. The term diffusion controlled kinetics is also used for this case. A general kinetic equation is

$$\alpha(t) = \frac{(k \cdot t)^n}{r}$$

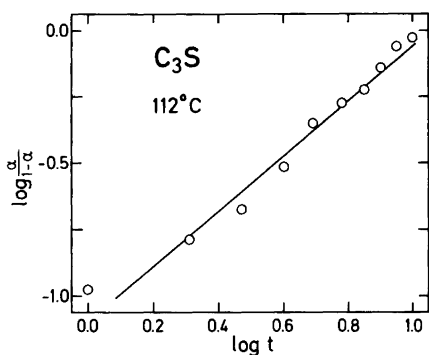


Fig. 7. Display of  $\log a/(1-\alpha)$  vs.  $\log t$  for the reaction of  $\text{C}_3\text{S}$  with  $\text{D}_2\text{O}$  at  $112^{\circ}\text{C}$ .

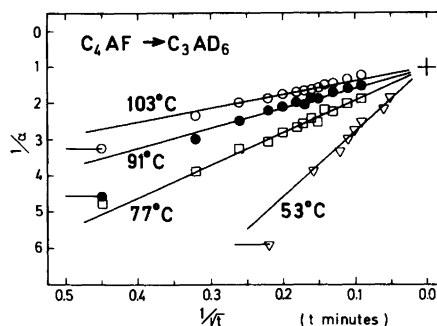


Fig. 8. The inverse degree of hydration ( $1/\alpha$ ) vs. the inverse square root of time ( $1/\sqrt{t}$ ) for reactions of  $\text{C}_4\text{AF}$  with  $\text{D}_2\text{O}$ .



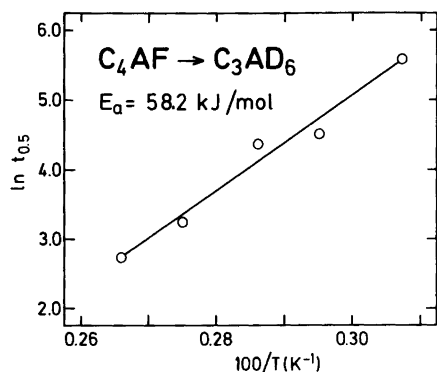


Fig. 9. Arrhenius plot of  $\ln t_{0.5}$  vs  $100/T$  for the formation of  $C_3AD_6$  from the reactions of  $C_4AF$  with  $D_2O$ . Estimated uncertainty in  $E_a$  10 %.

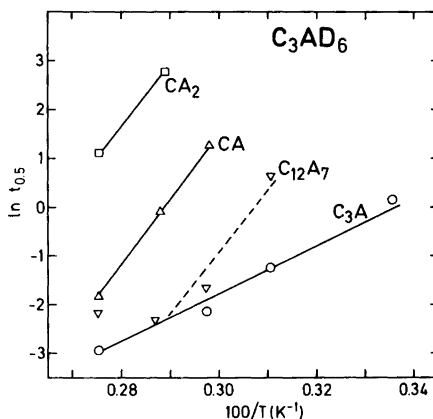


Fig. 10. Arrhenius plot of  $\ln t_{0.5}$  vs.  $100/T$  for production of the hydration product  $C_3AD_6$  in the reactions of  $C_3A$ ,  $C_{12}A_7$ ,  $CA$ , and  $CA_2$  with  $D_2O$ .

where  $k$  is a rate constant,  $t$  is time, and  $r$  is a measure of the particle size.<sup>29</sup> The linear kinetic corresponds to  $n=1$ , and the parabolic to  $n=\frac{1}{2}$ . A quantitative distinction between linear and parabolic kinetics can be obtained from plots of  $\log \alpha(t)$  vs.  $\log t$ , but for a qualitative distinction inspections of the  $\alpha(t)$  vs.  $t$  plots are sometimes sufficient. Figs. 2 and 6 represent linear and parabolic reaction kinetics of the hydration processes, respectively. When the polydispersity of the particles are included in the kinetic equation<sup>29</sup>

$$\alpha = \alpha(t) = \frac{t^n}{t^n + 1/BK^n}$$

where  $t$  is measured from the end  $t_0$  of any dormant period,  $B$  is a dispersion constant, and  $K$  a rate constant. The expression may be rewritten to

$$\log \alpha/(1-\alpha) = n \log (t-t_0) + \text{constant}$$

that can be used to estimate the value of  $n$ .

For a more detailed discussion,  $C_3S$  will first be considered. The hydration reaction of  $C_3S$  is characterized by a long induction period (here  $t_0=9$  h). Several model descriptions for the hydration of  $C_3S$  have been forwarded, however, it has been pointed out that conclusions based on details of the hydration [ $\alpha(t)$ ] curves are limited by dominating effects of the intrinsic particle size distribution.<sup>29</sup> Thus the data obtained for  $C_3S$  are analyzed according to the dispersion model.<sup>29</sup> For  $C_3S$  is a plot of  $\log \alpha/(1-\alpha)$  vs.  $\log t$  shown in Fig. 7 and the linear relationship (*viz.*  $n=1$ ) suggests reaction controlled kinetics.

The hydration curves of  $C_4AF$  differ from those of  $C_3S$  in the way that they have a negative curvature throughout the reaction period. The time dependance of  $\alpha(t)$  for  $C_4AF$  determined by the formation of  $C_3AD_6$  is shown in Fig. 8, where  $1/\alpha$  is plotted against  $1/\sqrt{t}$ . The data points fall on straight lines in accordance with a diffusion controlled kinetic description of the formation of  $C_3AD_6$  from  $C_4AF$ . Ideally, the lines should pass through the point  $1/\alpha=1$ ,  $1/t^{1/2}=0$ . They do so when the first data point of each measurement is omitted.

It seems acceptable to do so as these points are determined with the greatest uncertainty in  $t$  and  $\alpha$ .

The hydration of  $C_4AF$  was performed at different temperatures (Figs. 5,6) and the determinations of  $t_{0.5}$  were used to estimate the activation energy of the formation of  $C_3AD_6$  from  $C_4AF$  as 58.2 kJ/mol from an Arrhenius plot<sup>29</sup> of  $\ln t_{0.5}$  vs.  $100/T$ , see Fig. 9. Similar Arrhenius plots are shown in Fig. 10 for the hydration of the calcium aluminates, yielding activation energies for the reactions (formation of  $C_3AD_6$ ) as follows: For  $C_3A$  40 kJ/mol while for  $C_{12}A_7$ ,  $CA$  and  $CA_2$  approximately 105 kJ/mol. The variation in the derived values for the activation energies indicates probably that the reaction products, here including the amorphous gels, and hence the mechanisms are different for the phases studied.<sup>4</sup> The compounds with a high  $C/A$  ratio ( $C_3A$  and  $C_4AF$ ) apparently have low activation energies, and the compounds with low  $C/A$  ratio ( $C_{12}A_7$ ,  $CA$  and  $CA_2$ ) have high activation energies for the formation of  $C_3AD_6$ .

The large variations in reactivity of the various phases studied here [cf.  $t_{0.5}(\text{reactant})$  in Table 3] are believed to be reflected by details of the crystal structures. However, the properties of the amorphous intermediate gels may blurr any clear structural correlation with reactivity. By considering the stoichiometry of crystalline reactants and products it is evident that  $A$  rich gels prevail in the hydration products of  $C_{12}A_7$ ,  $CA$ , and  $CA_2$  while  $S$  rich gels are common for  $C_3S$  and  $\beta\text{-}C_2S$ . Only for  $C_3A$  the reactant and product ( $C_3AD_6$ ) have the same proportion of  $C$  and  $A$ .

For the  $C$ - $A$  compounds values for  $\ln t_{0.5}(\text{reactant})$  and various geometrical parameters are summarized in Fig. 11. A common feature of the crystal structures adopted by the reactant phases, is a framework of connected  $XO_4$  tetrahedra ( $X=\text{Al, Si, Fe}$ ), cf. e.g. the constancy of the averaged  $\text{Al}-\text{O}$  distances for calcium aluminates shown in Fig. 11. The coordination of  $\text{Ca}^{2+}$  with the oxygen atoms is less regular and the  $\text{Ca}-\text{O}$  distances vary considerably both within a given  $\text{CaO}_x$  polyhedron (from 2.258 to 2.569 Å for  $C_3A$ , from 2.360 to 2.523 Å for  $C_{12}A_7$ , etc.) and with the  $C/A$  ratio. The way of packing of the  $\text{AlO}_4$

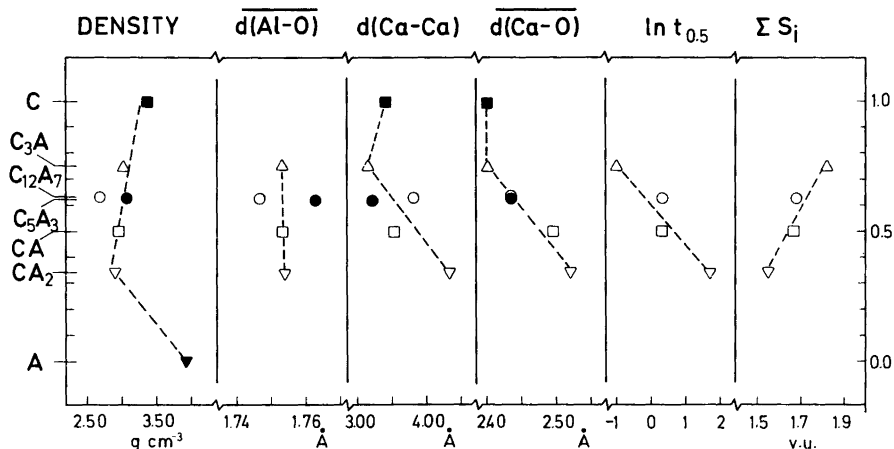


Fig. 11. Interatomic distances (mean  $\text{CaO}_6$ , mean  $\text{AlO}_4$ , shortest  $\text{Ca}-\text{Ca}$ ) for  $C_3A$ ,<sup>32</sup>  $C_{12}A_7$ ,<sup>33</sup>  $C_5A_3$ ,<sup>34</sup>  $CA$ ,<sup>35</sup>  $CA_2$ ,<sup>36</sup>  $A$ ,<sup>37</sup> and  $C_3A$ <sup>38</sup> as well as  $\log t_{0.5}$  and  $S_i$  for the  $\text{CaO}-\text{Al}_2\text{O}_3$  compounds. (The  $\text{Al}-\text{O}$  distances in  $\alpha\text{-Al}_2\text{O}_3$  are 1.86 and 1.97 Å). The symbols indicate  $C$  (■),  $C_3A$  (△),  $C_{12}A_7$  (○),  $C_5A_3$  (●),  $CA$  (□),  $CA_2$  (▽), and  $A$  (▼). The ordinate indicates mole fraction of compounds from pure  $A$  to pure  $C$ .

building blocks (tetrahedra) as well as the way of incorporation of  $\text{Ca}^{2+}$  into larger holes (channels) in the framework differ considerably between the *C-A* compounds. A high *C/A* ratio corresponds to a relative large fraction of the structure being occupied by  $\text{Ca}^{2+}$  ions and thus to a denser packing of these ions which in turn is reflected in the minimum Ca–Ca distance as well in the mean Ca–O bond lengths (see Fig. 11).

The reaction rates of the  $\text{Ca}_x\text{Al}_y\text{O}_z$  compounds with water thus appear to have the greatest values for the phases with the highest calcium content and appear to correlate with the shortest Ca–Ca distances and the average Ca–O distances of the phases (Fig. 11). The hypothesis was tested that a correlation to reactivity also existed with the total bond strength of the Ca–O bonds. The individual bond strength  $S_i$  introduced by Pauling<sup>30</sup> is related to the bond length using the expression employed by Brown and Shannon<sup>31</sup> as  $S_i = S_0(\bar{R}/R_i)^N$ , where  $R_i$  is the Ca–O distance and the other symbols have the values<sup>31</sup>  $S_0 = 0.25$  v.u. (valence units),  $N = 6$ , and  $\bar{R} = 2.468$  Å. The electrostatic valence principle<sup>30</sup> states that the sum of the bond strengths is equal to the valence. For  $\text{Ca}^{2+}$  the valence is expected to be 2 v.u. Fig. 11 shows bond strengths for  $\text{Ca}^{2+}$  between 1.55 and 1.82. Compounds with valence for calcium near the value 2 are expected to be the most stable, and an indication for this is found in the values of  $S_i$  for the two end products of the hydrolysis,  $\text{C}_3\text{AD}_6$  and  $\text{Ca}(\text{OD})_2$  with 1.84 and 1.95 v.u., respectively. The hypothesis of correlation between bond strength and reaction rate of hydrolysis can thus be rejected, as the reactivity of  $\text{C}_3\text{A}$  with water is greater than that of  $\text{CA}_2$ , while the calculated bond strength of the Ca–O bonds are greater in  $\text{C}_3\text{A}$  than in  $\text{CA}_2$ .

The structural properties of  $\text{Ca}^{2+}$  do not alone satisfactorily explain the observed trend in reactivity. Hence, properties connected with the  $\text{AlO}_4$ -tetrahedra probably also play an important role. A protonic attack on the surface has been suggested to be an important mechanism in the hydrolyses,<sup>19</sup> and the effective charge on the  $\text{AlO}_4$ -tetrahedra may be a relevant parameter. The result of the hydrolysis is a change of the coordination of Al from tetrahedral to octahedral coordination.

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