

## The Crystal and Molecular Structure of 1-Thiacyclobutane-3-carboxylic Acid-1-oxide

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The high melting isomer of 1-thiacyclobutane-3-carboxylic acid-1-oxide ( $C_4H_6O_3S$ ) is orthorhombic ( $Pna2_1$ ) with  $a = 9.89 \pm 0.05$ ,  $b = 5.41 \pm 0.02$ , and  $c = 10.81 \pm 0.08$  Å. The molecule has the *trans* configuration and shows a puckered four membered ring (dihedral angle  $153^\circ$ ). The molecules are held together by hydrogen bonds between the carboxyl and sulphoxide groups.

1-Thiacyclobutane-3-carboxylic acid-1-oxide ( $C_4H_6O_3S$ ) was prepared by Allenmark.<sup>1</sup> He found that the synthetic product had a diffuse melting point and interpreted this as due to the presence of the geometric isomers which are possible because of the ring system. A separation of the two forms was possible by repeated recrystallization from ethyl acetate or acetone. One modification melted at  $130.5 - 133.0^\circ C$  whereas the other (isolated from the mother liquor) melted between  $133^\circ C$  and  $138^\circ C$ . Crystals from the high melting form were used for a crystal structure determination.

### EXPERIMENTAL

Crystals of  $C_4H_6O_3S$  are orthorhombic ( $Pna2_1$ ) with the following unit cell dimensions:  $a = 9.89 \pm 0.05$ ,  $b = 5.41 \pm 0.02$ , and  $c = 10.81 \pm 0.08$  Å. The intensity data were collected with the Weissenberg technique using  $CuK\alpha$  radiation. Rotation about the *b*-axis gave layers 0-4, and about the *c*-axis layers 0-7. The film intensities were measured on the automatic film scanner<sup>2</sup> developed at this institute. They were then scaled<sup>3</sup> together to a set of 532 independent reflexions. The intensities were corrected for the Lorentz and polarization factors but not for absorption.

### STRUCTURE DETERMINATION

The sulphur atom was found from a sharpened Patterson series and the remaining atoms were then located from successive electron density and difference syntheses. The hydrogen atom of the carboxyl group was found at the expected position but was poorly defined. This has been the case in rather

Table 1. Observed and calculated structure factors. The phase angles are given as fractions of one revolution.

H	K	L	Fobs	Fcalc	FI	H	K	L	Fobs	Fcalc	FI	H	K	L	Fobs	Fcalc	FI			
0	0	2	356	518	0.118	1	5	4	55	54	0.435	3	1	8	47	50	0.517			
0	0	4	294	421	0.822	1	1	5	19	18	0.808	1	1	9	123	122	0.330			
0	0	6	251	279	0.899	1	1	5	73	71	0.479	1	1	10	63	58	0.935			
0	0	8	180	191	0.062	1	1	1	35	36	0.697	1	1	11	147	133	0.275			
0	0	10	217	226	0.931	1	1	6	0	40	0.500	2	2	2	519	474	0.500			
0	0	12	132	132	0.061	1	1	6	1	33	0.309	2	2	2	132	104	0.673			
0	1	3	259	266	0.076	2	0	3	27	37	0.433	2	2	2	128	110	0.504			
0	1	5	418	407	0.226	2	0	0	41	26	0.500	2	2	2	92	79	0.520			
0	1	7	212	182	0.357	2	0	1	393	508	0.115	2	2	2	270	252	0.513			
0	1	9	85	71	0.908	2	0	3	373	514	0.339	2	2	2	63	64	0.227			
0	1	11	108	99	0.198	2	0	4	230	270	0.087	2	2	2	152	160	0.512			
0	2	2	704	604	0.000	2	0	5	196	247	0.252	2	2	2	44	38	0.116			
0	2	2	363	359	0.920	2	0	6	100	98	0.383	2	2	2	147	133	0.275			
0	2	2	229	234	0.016	2	0	7	181	207	0.196	2	2	2	24	30	0.674			
0	2	4	6	93	0.742	2	0	8	197	224	0.168	2	2	2	142	131	0.449			
0	2	8	135	138	0.993	2	0	9	253	271	0.292	2	2	2	11	25	0.634			
0	2	10	115	104	0.961	2	0	10	112	110	0.116	2	2	2	158	138	0.000			
0	2	12	54	46	0.980	2	0	11	38	43	0.375	2	2	2	96	87	0.851			
0	3	1	263	226	0.379	2	0	12	78	68	0.956	2	2	2	51	44	0.133			
0	3	3	331	319	0.190	2	1	1	263	240	1.000	2	2	2	86	86	0.223			
0	3	3	362	362	0.000	2	1	1	64	64	0.796	2	2	2	80	73	0.512			
0	3	3	258	234	0.254	2	1	2	417	441	0.418	2	2	2	78	76	0.514			
0	3	5	61	50	0.132	2	1	3	188	274	0.332	2	2	2	50	44	0.689			
0	3	11	116	90	0.220	2	1	4	220	231	0.597	2	2	2	34	33	0.313			
0	4	4	271	219	0.500	2	1	1	140	133	0.541	2	2	2	41	41	0.015			
0	4	4	94	96	0.234	2	1	5	48	37	0.638	2	2	2	47	44	0.427			
0	4	4	84	98	0.494	2	1	6	148	134	0.108	2	2	2	264	244	0.500			
0	4	4	81	98	0.703	2	1	7	124	111	0.425	2	2	2	86	77	0.738			
0	4	8	10	25	0.477	2	1	8	92	82	0.279	2	2	2	147	134	0.505			
0	4	10	57	49	0.140	2	1	9	74	69	0.570	2	2	2	32	30	0.381			
0	4	11	203	190	0.247	2	1	10	48	45	0.412	2	2	2	196	181	0.573			
0	4	15	69	68	0.335	2	2	0	195	175	0.000	2	2	2	51	27	0.271			
0	4	17	131	127	0.157	2	2	1	207	176	0.190	2	2	2	76	74	0.660			
0	4	19	104	91	0.500	2	2	2	125	113	0.701	2	2	2	26	26	0.184			
0	4	2	99	104	0.446	2	2	3	113	103	0.315	2	2	2	126	132	0.521			
0	4	4	86	94	0.555	2	2	3	88	78	0.839	2	2	2	12	18	0.816			
0	4	0	436	446	1.000	2	2	2	224	221	0.215	2	2	2	30	25	0.000			
1	1	1	623	622	0.300	2	2	2	79	78	0.188	2	2	2	124	101	0.780			
1	1	1	2	566	623	0.973	2	2	7	116	102	0.355	2	2	2	26	27	0.271		
1	1	1	3	308	316	0.244	2	2	7	127	131	0.184	2	2	2	100	98	0.718		
1	1	1	4	175	203	0.778	2	2	9	91	79	0.273	2	2	2	75	80	0.756		
1	1	1	5	30	29	0.174	2	2	10	65	56	0.064	2	2	2	16	21	0.919		
1	1	1	6	209	209	0.063	2	2	11	45	48	0.257	2	2	2	71	78	0.720		
1	1	1	7	172	189	0.104	2	2	12	35	45	0.030	2	2	2	42	39	0.500		
1	1	1	8	165	163	0.037	2	2	1	83	69	0.500	2	2	2	18	22	0.794		
1	1	1	9	122	107	0.158	2	2	1	148	133	0.190	2	2	2	18	22	0.794		
1	1	1	10	164	149	0.072	2	2	2	400	357	0.478	2	2	2	13	19	0.132		
1	1	1	11	67	65	0.262	2	2	3	191	188	0.359	2	2	2	23	35	0.693		
1	1	1	12	110	91	0.947	2	2	3	170	164	0.529	2	2	2	79	82	0.500		
1	1	2	0	20	8	0.500	2	2	5	124	115	0.415	2	2	2	485	582	0.271		
1	1	2	2	222	197	0.153	2	2	6	158	149	0.544	2	2	2	273	290	0.780		
1	1	2	2	341	308	0.332	2	2	6	156	143	0.164	2	2	2	137	138	0.424		
1	1	2	3	345	315	0.365	2	2	6	149	128	0.453	2	2	2	229	237	0.613		
1	1	2	4	310	324	0.501	2	2	9	99	80	0.237	2	2	2	361	417	0.184		
1	1	2	5	307	293	0.247	2	2	10	135	106	0.531	2	2	2	189	217	0.466		
1	1	2	6	89	80	0.530	2	2	11	58	54	0.266	2	2	2	136	146	0.351		
1	1	2	7	157	142	0.249	2	2	4	31	31	0.000	2	2	2	123	141	0.540		
1	1	2	8	34	35	0.528	2	2	4	91	75	0.652	2	2	2	140	148	0.140		
1	1	2	9	131	125	0.205	2	2	4	2	115	108	0.402	2	2	2	58	65	0.542	
1	1	2	10	48	48	0.398	2	2	4	3	117	108	0.820	2	2	2	11	120	0.231	
1	1	2	11	55	54	0.215	2	2	4	4	94	90	0.587	2	2	2	239	270	0.500	
1	1	2	12	22	30	0.562	2	2	4	5	20	21	0.206	2	2	2	88	106	0.644	
1	1	3	0	28	29	0.000	2	2	4	6	39	42	0.175	2	2	2	173	180	0.656	
1	1	3	1	114	97	0.334	2	2	4	7	86	81	0.599	2	2	2	140	144	0.630	
1	1	3	2	98	95	0.861	2	2	4	8	47	49	0.375	2	2	2	182	180	0.277	
1	1	3	3	49	46	0.183	2	2	4	9	66	68	0.785	2	2	2	46	55	0.843	
1	1	3	4	40	38	0.807	2	2	5	0	180	157	0.500	2	2	2	187	201	0.323	
1	1	3	5	47	46	0.190	2	2	5	1	122	110	0.425	2	2	2	56	59	0.915	
1	1	3	6	77	71	0.206	2	2	5	2	125	122	0.637	2	2	2	33	28	0.674	
1	1	3	7	25	25	0.128	2	2	5	3	39	40	0.512	2	2	2	19	19	0.737	
1	1	3	8	33	32	0.952	2	2	5	4	46	41	0.287	2	2	2	55	53	0.439	
1	1	3	9	201	29	0.994	2	2	5	5	58	63	0.273	2	2	2	11	70	0.732	
1	1	3	10	29	30	0.040	2	2	5	6	87	94	0.519	2	2	2	82	72	0.000	
1	1	3	11	25	26	0.040	2	2	5	6	31	42	0.300	2	2	2	221	208	0.203	
1	1	4	0	148	123	0.500	2	2	6	0	82	80	0.500	2	2	2	88	78	0.874	
1	1	4	1	148	129	0.236	2	2	6	0	86	82	0.751	2	2	2	198	194	0.348	
1	1	4	2	86	80	0.396	2	2	6	2	19	24	0.489	2	2	2	167	160	0.587	
1	1	4	3	182	178	0.362	2	2	6	2	148	148	0.750	2	2	2	107	110	0.232	
1	1	4	4	134	142	0.455	2	2	6	3	47	54	0.406	2	2	2	103	105	0.527	
1	1	4	5	201	182	0.235	2	2	6	4	221	221	0.000	2	2	2	68	68	0.158	
1	1	4	6	96	95	0.464	2	2	6	5	348	347	0.407	2	2	2	61	55	0.583	
1	1	4	7	113	102	0.246	2	2	6	6	249	260	0.854	2	2	2	9	125	0.211	
1	1	4	8	63	59	0.569	2	2	6	7	248	268	0.176	2	2	2	10	46	0.592	
1	1	4	9	112	95	0.210	2	2	6	7	102	100	0.628	2	2	2	11	27	0.275	
1	1	4	10	117	100	0.800	2	2	6	8	251	260	0.332	2	2	2	0	183	164	0.500
1	1	4	11	76	57	0.802	2	2	6	9	123	124	0.447	2	2	2	1	200	161	0.743
1	1	4	12	108	105	0.513	2													

Table 1. Continued.

H	K	L	Fobs	Fcalc	FI	H	K	L	Fobs	Fcalc	FI	H	K	L	Fobs	Fcalc	FI
4	4	3	152	127	0.670	6	1	6	50	53	0.096	8	1	2	108	100	0.101
4	4	4	168	159	0.387	6	1	7	92	95	0.653	8	1	3	32	29	0.442
4	4	5	44	42	0.880	6	1	8	23	26	0.402	8	1	4	25	26	0.981
4	4	6	213	222	0.26	6	1	9	87	83	0.807	8	1	5	23	27	0.598
4	4	7	68	74	0.854	6	1	10	21	23	0.666	8	1	6	73	69	0.990
4	4	8	84	75	0.513	6	1	11	171	175	0.500	8	1	7	39	38	0.819
4	4	9	79	66	0.777	6	2	1	75	77	0.758	8	1	8	47	52	0.974
4	4	10	88	74	0.516	6	2	2	101	98	0.583	8	2	0	25	19	0.500
4	4	11	120	99	0.000	6	2	3	26	22	0.803	8	2	1	75	68	0.655
4	4	12	84	72	0.864	6	2	4	196	198	0.520	8	2	2	65	57	0.733
4	4	13	59	57	0.108	6	2	5	15	26	0.227	8	2	3	68	53	0.745
4	4	14	44	40	0.356	6	2	6	125	137	0.435	8	2	4	80	77	0.623
4	4	15	23	12	0.779	6	2	7	44	44	0.444	8	2	5	85	82	0.759
4	4	16	92	93	0.683	6	2	8	84	75	0.468	8	2	6	34	29	0.466
4	4	17	46	47	0.904	6	2	9	42	45	0.386	8	2	7	57	63	0.852
4	4	18	60	64	0.938	6	2	10	37	28	0.500	8	2	8	37	39	0.462
4	4	19	42	41	0.954	6	2	11	230	237	0.749	8	2	9	154	136	0.000
4	4	20	35	20	0.461	6	2	12	39	42	0.678	8	2	10	98	83	0.794
4	4	21	35	33	0.000	6	2	13	238	227	0.691	8	2	11	172	150	0.074
4	4	22	175	73	0.792	6	2	14	84	81	0.692	8	2	12	66	62	0.576
4	4	23	147	145	0.410	6	2	15	72	66	0.783	8	2	13	75	71	0.731
4	4	24	34	21	0.794	6	2	16	45	45	0.077	8	2	14	26	32	0.745
4	4	25	81	93	0.528	6	2	17	129	129	0.711	8	2	15	106	95	0.009
4	4	26	23	22	0.162	6	2	18	108	94	0.797	8	2	16	52	52	0.828
4	4	27	38	46	0.541	6	2	19	25	22	0.500	8	2	17	28	28	0.000
4	4	28	28	31	0.773	6	2	20	53	54	0.427	8	2	18	42	35	0.239
4	4	29	42	42	0.000	6	2	21	72	73	0.984	8	2	19	46	46	0.000
4	4	30	109	114	0.500	6	2	22	39	39	0.784	8	2	20	39	39	0.858
4	4	31	121	125	0.244	6	2	23	68	69	0.094	8	2	21	47	51	0.241
4	4	32	318	383	0.567	6	2	24	21	20	0.012	8	2	22	40	35	1.000
4	4	33	238	261	0.206	6	2	25	23	21	0.315	8	2	23	144	128	0.758
4	4	34	212	217	0.556	6	2	26	8	25	0.978	8	2	24	51	54	0.641
4	4	35	87	95	0.315	6	2	27	28	31	0.500	8	2	25	168	161	0.732
4	4	36	184	193	0.482	6	2	28	91	103	0.783	8	2	26	59	43	0.500
4	4	37	110	121	0.138	6	2	29	13	24	0.781	8	2	27	46	46	0.000
4	4	38	134	183	0.383	6	2	30	67	74	0.641	8	2	28	61	58	0.255
4	4	39	30	33	0.185	6	2	31	9	58	0.724	8	2	29	87	86	0.742
4	4	40	98	94	0.503	6	2	32	56	54	0.000	8	2	30	122	104	0.000
4	4	41	43	40	0.115	6	2	33	149	146	0.741	8	2	31	85	78	0.469
4	4	42	0	175	0.500	6	2	34	129	119	0.580	8	2	32	104	93	0.992
4	4	43	269	271	0.626	6	2	35	159	152	0.689	8	2	33	42	45	0.621
4	4	44	101	106	0.476	6	2	36	181	179	0.477	8	2	34	119	120	0.053
4	4	45	237	240	0.709	6	2	37	86	80	0.696	8	2	35	42	41	0.287
4	4	46	90	79	0.585	6	2	38	238	251	0.554	8	2	36	74	75	0.946
4	4	47	139	143	0.734	6	2	39	90	94	0.736	8	2	37	11	12	0.310
4	4	48	90	101	0.268	6	2	40	41	46	0.521	8	2	38	59	43	0.500
4	4	49	64	70	0.803	6	2	41	27	35	0.770	8	2	39	81	69	0.875
4	4	50	124	119	0.507	6	2	42	112	109	0.000	8	2	40	25	30	0.776
4	4	51	120	110	0.776	6	2	43	267	260	0.778	8	2	41	29	30	0.148
4	4	52	68	61	0.500	6	2	44	110	103	0.014	8	2	42	29	35	0.371
4	4	53	126	123	0.361	6	2	45	43	37	0.996	8	2	43	20	31	0.504
4	4	54	100	98	0.689	6	2	46	87	76	0.448	8	2	44	88	80	0.000
4	4	55	23	22	0.760	6	2	47	113	115	0.633	8	2	45	55	51	0.988
4	4	56	59	63	0.127	6	2	48	78	73	0.907	8	2	46	33	42	0.441
4	4	57	48	52	0.470	6	2	49	75	76	0.845	8	2	47	115	115	0.000
4	4	58	17	23	0.208	6	2	50	65	66	0.004	8	2	48	160	160	0.688
4	4	59	30	30	0.998	6	2	51	103	87	0.735	8	2	49	100	100	0.937
4	4	60	134	133	0.500	6	2	52	67	70	0.000	8	2	50	136	140	0.756
4	4	61	164	170	0.685	6	2	53	27	26	0.795	8	2	51	40	48	0.052
4	4	62	48	45	0.452	6	2	54	36	37	0.483	8	2	52	55	78	0.723
4	4	63	114	116	0.679	6	2	55	39	39	0.582	8	2	53	27	24	0.139
4	4	64	109	99	0.433	6	2	56	56	53	0.705	8	2	54	23	24	1.000
4	4	65	127	139	0.702	6	2	57	20	22	0.713	8	2	55	33	29	0.332
4	4	66	52	58	0.479	6	2	58	18	20	0.279	8	2	56	73	63	0.989
4	4	67	81	88	0.841	6	2	59	32	49	0.500	8	2	57	39	39	0.362
4	4	68	28	29	0.573	6	2	60	98	94	0.000	8	2	58	36	39	0.011
4	4	69	41	70	0.807	6	2	61	137	141	0.695	8	2	59	55	29	0.232
4	4	70	60	58	0.000	6	2	62	63	60	0.022	8	2	60	39	39	0.974
4	4	71	28	23	0.791	6	2	63	105	98	0.800	8	2	61	100	85	0.000
4	4	72	72	74	0.031	6	2	64	58	65	0.004	8	2	62	115	99	0.721
4	4	73	35	34	0.678	6	2	65	30	34	0.784	8	2	63	42	38	0.005
4	4	74	39	51	0.330	6	2	66	71	63	0.500	8	2	64	71	62	0.760
4	4	75	23	26	0.819	6	2	67	25	34	0.752	8	2	65	62	53	0.687
4	4	76	21	56	0.005	6	2	68	24	21	1.000	8	2	66	53	47	0.000
4	4	77	171	159	0.500	6	2	69	41	40	0.268	8	2	67	29	34	0.345
4	4	78	245	267	0.845	6	2	70	17	57	0.967	8	2	68	99	98	0.992
4	4	79	234	231	0.453	6	2	71	19	31	0.250	8	2	69	35	66	0.302
4	4	80	76	69	0.207	6	2	72	63	63	0.000	8	2	70	69	69	0.983
4	4	81	430	475	0.550	6	2	73	130	136	0.664	8	2	71	75	75	0.000
4	4	82	73	69	0.424	6	2	74	101	98	0.785	8	2	72	118	118	0.000
4	4	83	169	186	0.433	6	2	75	111	136	0.710	8	2	73	53	57	0.795
4	4	84	45	50	0.524	6	2	76	125	128	0.562	8	2	74	127	135	0.957
4	4	85	173	185	0.454	6	2	77	196	206	0.752	8	2	75	61	56	0.572
4	4	86	75	76	0.444	6	2	78	87	92	0.539	8	2	76	96	79	0.934
4	4	87	141	147	0.721	6	2	79	116	126	0.876	8	2	77	67	67	0.000
4	4	88	44	39	0.573	6	2	80	43	44	0.506	8	2	78	75	72	0.275
4	4	89	172	172	0.711	6	2	81	83	83	0.793	8	2	79	26	38	0.923
4	4	90	73	71	0.891	6	2	82	131	113	0.000	8	2	80	1	1	0.951
4	4	91	28	24	0.970	6	2	83	89	89	0.839	8	2	81	102	102	0.000

any structures with hydrogen bonding both with film scanner and diffractometer data. All hydrogen atoms were, however, included in the following structure factor calculations at their calculated positions with isotropic temperature factors corresponding to those of the parent atom. The refinement was performed by least-squares using anisotropic thermal parameters for all non-hydrogen atoms. The hydrogen parameters were not varied. The final *R*-value is 0.097 for all observed independent reflexions. In the refinement the residual  $\sum w (|F_o| - |k|F_c)^2$  was minimized where the weight *w* was

$$1 + \left( \frac{|F_o| - 4.42|F_{\min}|}{6.19|F_{\min}|} \right)^2$$

The form factors of the International Tables for X-Ray Crystallography<sup>4</sup> were used. The calculations were performed with the program system of Abrahamsson *et al.*<sup>5</sup>

## RESULTS

A list of the final set of observed and calculated structure factors is given in Table 1, the atomic parameters in Tables 2 and 3. The interatomic distances and angles are shown in Fig. 1, and with standard deviations in Table 4. There are no unexpected features in these values.

Table 2. Fractional coordinates for the atoms of the structure. The standard deviations (within brackets) are multiplied by 10<sup>4</sup> for *x*, *y*, and *z*, respectively.

	<i>x</i>	$\sigma(x)$	<i>y</i>	$\sigma(y)$	<i>z</i>	$\sigma(z)$	<i>B</i> (Å <sup>2</sup> )
S (1)	0.08491	(2)	1.07513	(4)	0.00041	(0)	
C (1)	0.26706	(13)	1.03379	(27)	-0.03464	(12)	
C (2)	0.29227	(11)	0.94342	(19)	0.09476	(14)	
C (3)	0.14365	(11)	0.87000	(22)	0.12383	(14)	
C (4)	0.33843	(11)	1.14552	(22)	0.18207	(11)	
O (1)	-0.00559	(9)	0.93981	(15)	-0.09174	(11)	
O (2)	0.42151	(9)	1.06842	(18)	0.27195	(12)	
O (3)	0.30000	(11)	1.35747	(16)	0.17275	(11)	
H(11)	0.29060		0.88400		-0.10610		4.07
H(12)	0.32570		1.19440		-0.06200		4.07
H(21)	0.37100		0.80740		0.10340		3.17
H(31)	0.12250		0.67040		0.10820		3.65
H(32)	0.10930		0.91590		0.21710		3.65
H(24)	0.46140		1.20030		0.33960		4.65

Table 3. Anisotropic thermal parameters  $\exp[-2\pi^2(U_{11}h^2a^{*2} + U_{22}k^2b^{*2} + U_{33}l^2c^{*2} + 2U_{23}klb^*c^* + 2U_{31}lhc^*a^* + 2U_{12}hka^*b^*)]$ .

	<i>U</i> <sub>11</sub>	<i>U</i> <sub>22</sub>	<i>U</i> <sub>33</sub>	<i>U</i> <sub>23</sub>	<i>U</i> <sub>31</sub>	<i>U</i> <sub>12</sub>
S(1)	0.03491	0.04201	0.03670	-0.00296	0.00085	0.00291
C(1)	0.04208	0.07829	0.03735	-0.02307	0.00522	-0.00529
C(2)	0.03381	0.03960	0.05260	-0.00706	0.00351	0.00145
C(3)	0.03776	0.04641	0.05848	0.00060	-0.00309	-0.00084
C(4)	0.03748	0.04711	0.03179	-0.00663	-0.00362	0.00374
O(1)	0.03306	0.06287	0.06432	-0.01514	-0.00061	-0.00235
O(2)	0.05733	0.05710	0.06293	-0.00645	-0.01754	0.00870
O(3)	0.07737	0.03495	0.06616	-0.00076	-0.02431	0.01350

Table 4. Interatomic distances and angles with e.s.d.'s.

S(1)–C(1)	= 1.854 Å	(0.012)
–C(3)	= 1.830	(0.013)
–O(1)	= 1.526	(0.010)
C(1)–C(2)	= 1.503	(0.017)
C(2)–C(3)	= 1.555	(0.014)
–C(4)	= 1.515	(0.015)
C(4)–O(2)	= 1.339	(0.015)
–O(3)	= 1.212	(0.014)
O(1)–S(1)–C(1)	= 112.2°	(0.6)
O(1)–S(1)–C(3)	= 111.8	(0.5)
C(1)–S(1)–C(3)	= 76.6	(0.5)
S(1)–C(1)–C(2)	= 90.6	(0.7)
C(1)–C(2)–C(3)	= 96.6	(0.9)
C(1)–C(2)–C(4)	= 113.3	(0.9)
C(3)–C(2)–C(4)	= 110.1	(0.9)
S(1)–C(3)–C(2)	= 89.8	
C(2)–C(4)–O(3)	= 122.4	(1.0)
C(2)–C(4)–O(2)	= 114.3	(0.9)
O(2)–C(4)–O(3)	= 123.2	(1.1)

From the stereoscopic drawing given in Fig. 2 it is obvious that the high melting form of  $C_4H_6O_3S$  has the *trans* configuration.

The four membered ring is non-planar. The dihedral angle between the planes defined by C(1), S(1), C(3) and C(1), C(2), C(3) is  $153^\circ$ , which agrees well with the values usually found in puckered cyclobutane rings.<sup>6</sup> The carboxyl group is roughly perpendicular to the four membered ring. The angle between the planes C(1), C(2), C(3) and O(2), C(4), O(3) is  $98^\circ$ .

The packing of the molecules is shown in Fig. 3. The molecules are linked together by hydrogen bonds between the carboxyl and the sulphoxide group. The I O(1) and III O(2) distance is 2.63 Å. The other intermolecular contacts

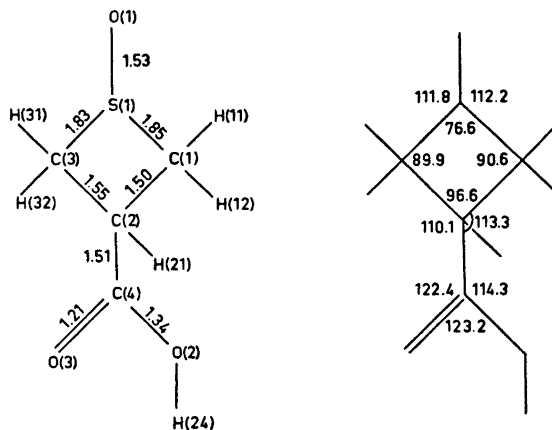


Fig. 1. Interatomic distances and angles of  $C_4H_6O_3S$ . The atomic numbering is also indicated.

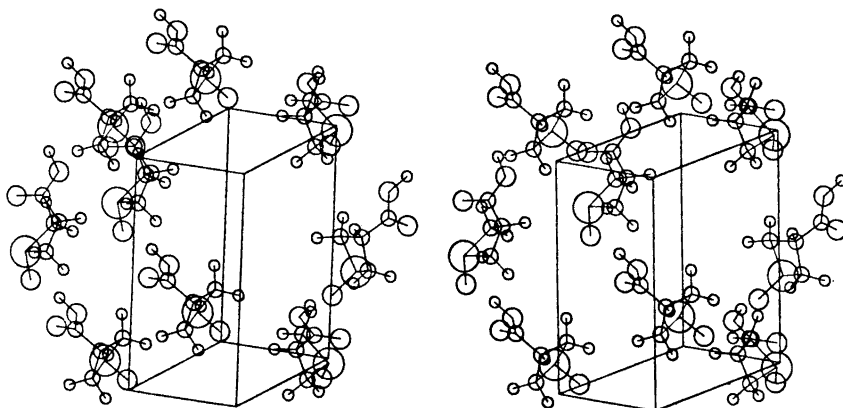


Fig. 2. Stereoscopic pair of  $C_4H_6O_3S$ .

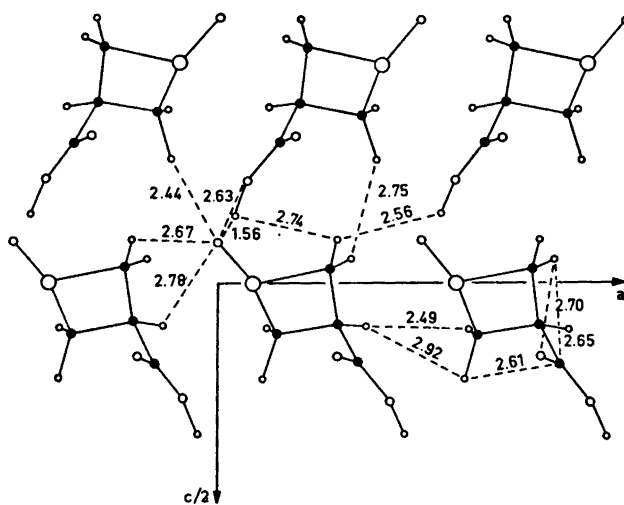


Fig. 3. Molecular packing of  $C_4H_6O_3S$ . Some short intra- and intermolecular contacts are shown.

as well as the nonbonded intramolecular distances indicate normal packing conditions.

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